



Spatially Targeted Activation of a SMP Based Reconfigurable Skin System

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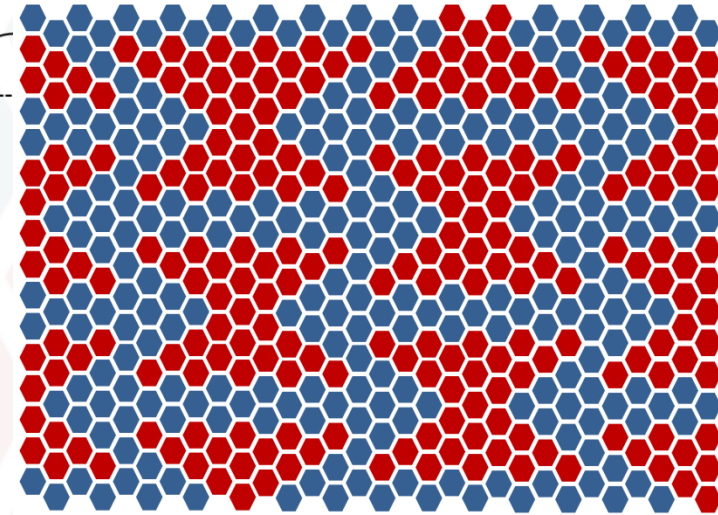
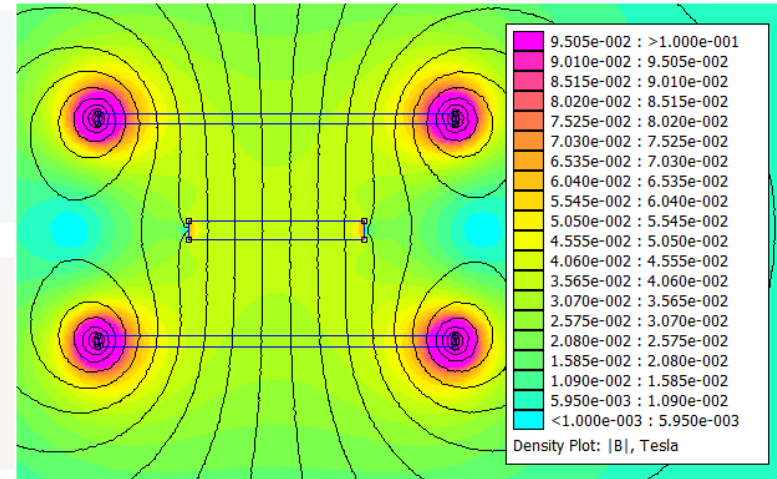
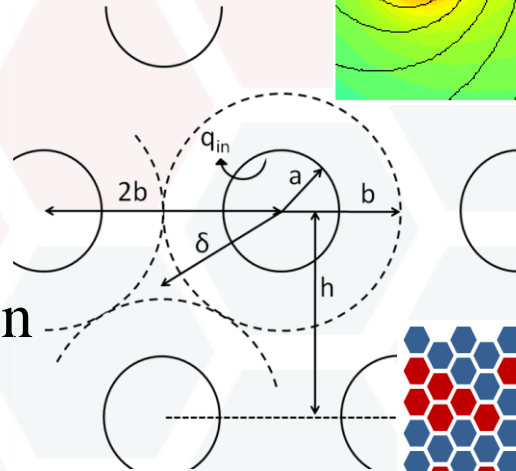


Overview



Adaptive Structures Team

- Project Overview
- Thermal
 - Thermal Modeling
 - Magnetic Modeling
 - Particle Alignment
- Mechanical
 - SMP Characterization
 - Constitutive Model
 - Geometry Optimization
- Future Work
- Summary



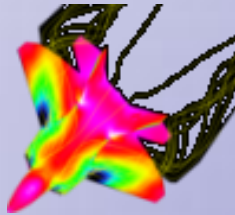


RQ Tech Division Consolidation



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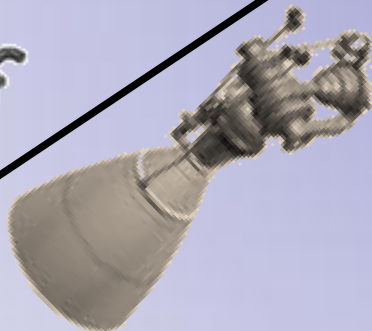
Aerospace Vehicles



High Speed Systems



Power and Control



Rocket Propulsion



Turbine Engine

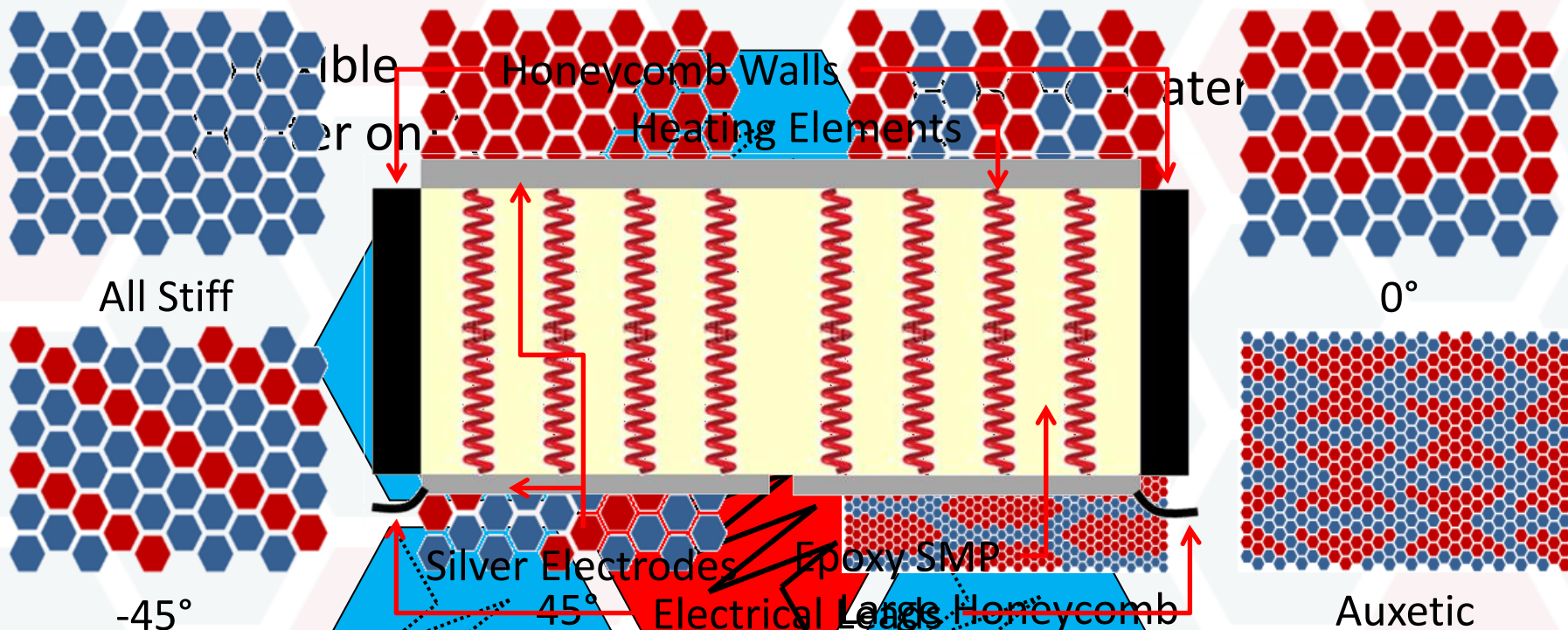




Project Overview



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Skin Objectives (via MAS)

- Formal Panel Size 15" x 20"
- Thermal diffusion between cells
- System wrinkling of skin
- Total skin weight 1095 lb/sqft
- System weight Load 400lb/sqft
- Max Out of Plane Deflection

Stiff (heater off)



Heating Options



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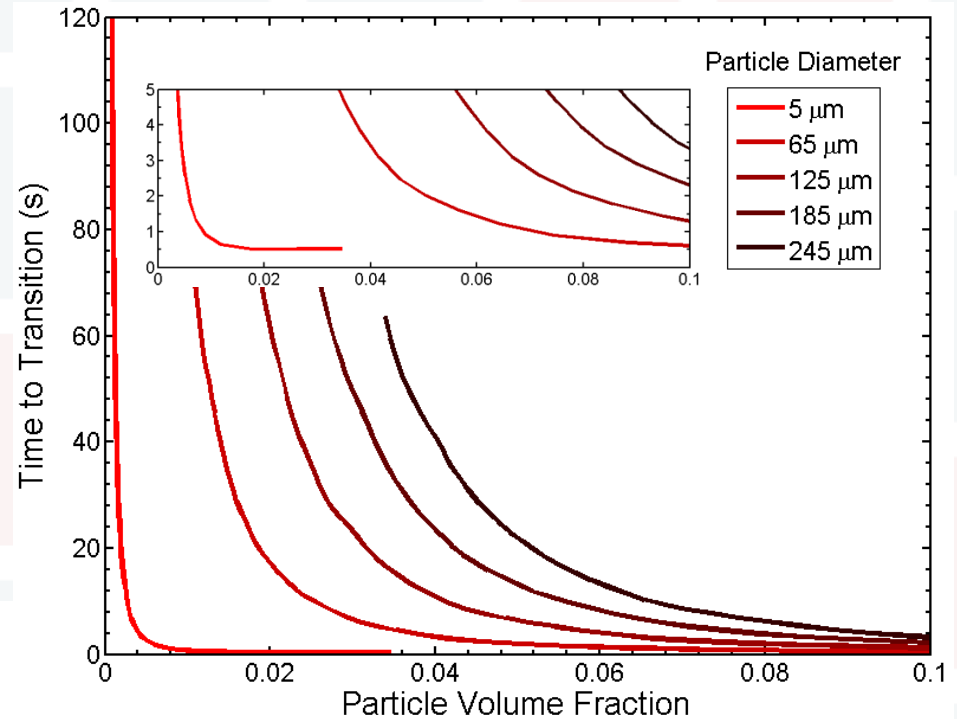
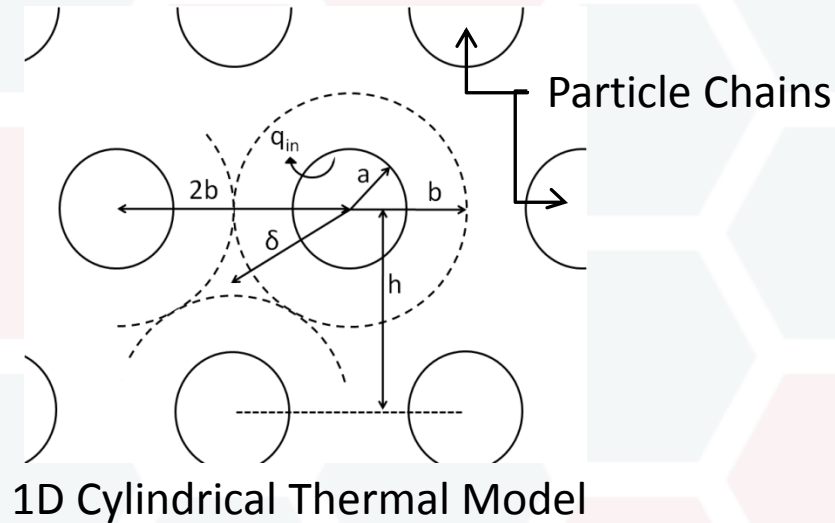
	Strain Capability	Corrosion Resistance	Conductivity	Manufacturability
NiChrome Mesh				
Permalloy80 Particle Chains				
Permalloy80 Random Particles				
NiChrome Wire Coils				
Stainless Steel Wool				
Constantine Wool				
Nickel Random Particles				
Nickel Particle Chains				



Thermal: Modeling



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- Surface temp of chain limited to service temp of SMP
- Reduction in power required to prevent damage to SMP
- Builds on previous results of temperature varying thermal properties

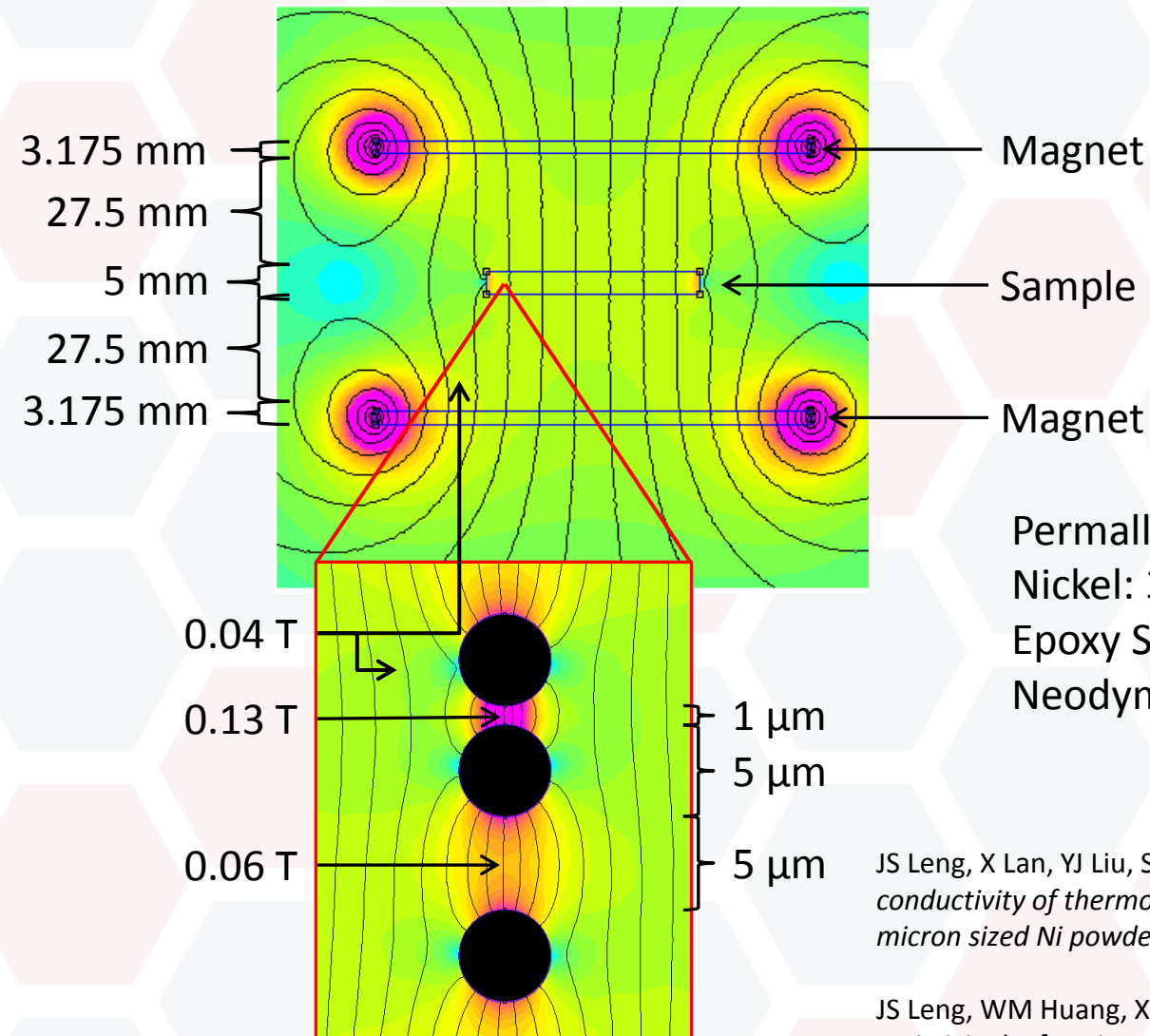


Thermal: Magnetic Alignment of Particles



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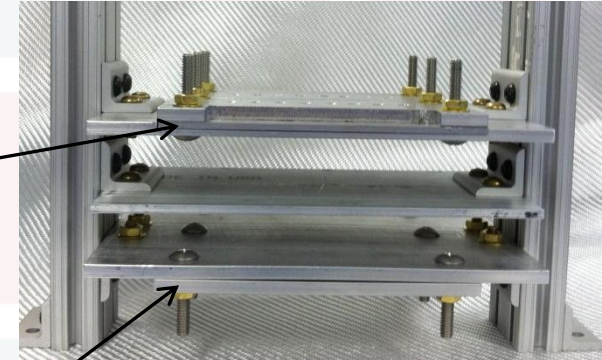
Magnetic Field Lines Between Two Magnets



Magnet

Sample

Magnet



Permalloy 80 (NiMoFe): 37 μm diameter

Nickel: 3-7 μm diameter

Epoxy SMP

Neodymium (NdFeB) N42SH magnets

JS Leng, X Lan, YJ Liu, SY Du, WN Huang, N Liu, SJ Phee, Q Yuan, *Electrical conductivity of thermoresponsive shape memory polymer with embedded micron sized Ni powder chains*, Applied Physics Letters, vol. 92, 2008

JS Leng, WM Huang, X Lan, YJ Liu, SY Du, *Significantly reducing electrical resistivity by forming conductive Ni chains in a polyurethane shape memory polymer/carbon black composite*, Applied Physics Letters, vol. 92, 2008

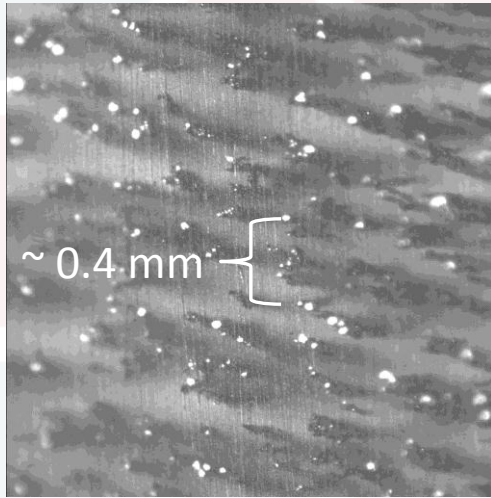
Magnetic Field Lines b/t Ni Particles



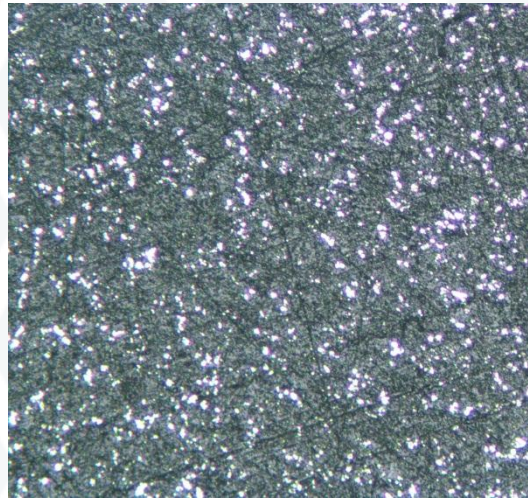
Thermal: Magnetic Alignment of Particles



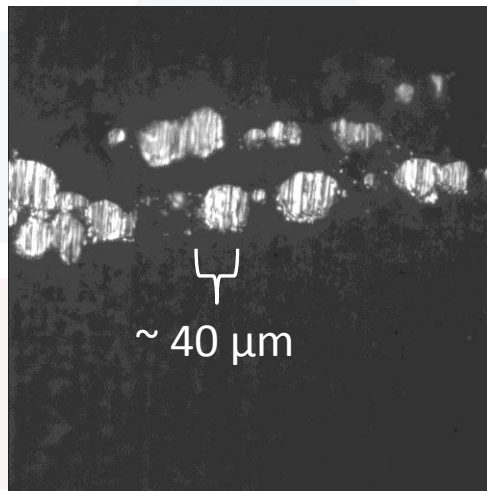
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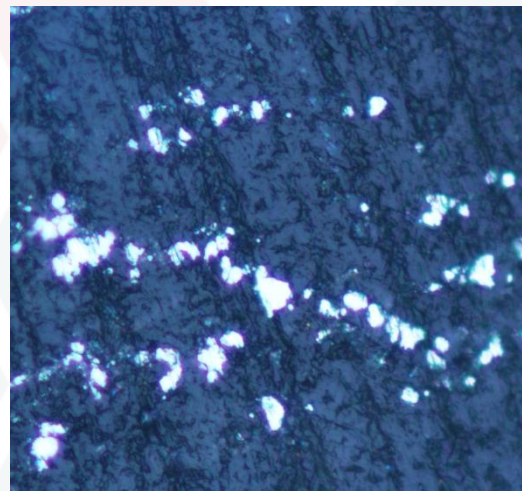
End View of Permalloy80



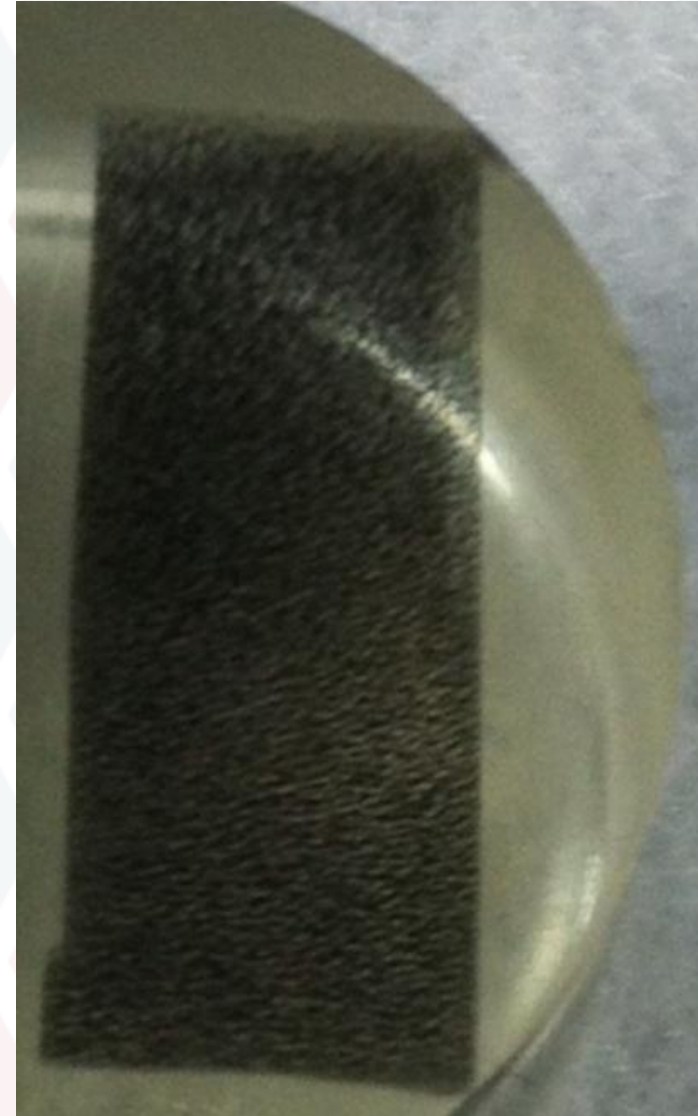
End View of Nickel



Side View Permalloy80



Side View Nickel



End View of Particle Chains



Thermal: Current Results



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Material	Diameter	Resistivity (Ω)	Comments
Permalloy80 Particles (random)	$\sim 37 \mu\text{m}$		Oxidized
Permalloy80 Particles (aligned)	$\sim 37 \mu\text{m}$		Oxidized
Ni-Cr Coil	0.3 mm	NA	Difficult to Manufacture
Nickel Particles (random)	3-7 μm	80	Viable Option
Stainless Steel Wool	0.08 mm	65	Viable Option
Nickel Particles (aligned)	3-7 μm	18	Viable Option
Constantine Wire Wool	0.02 mm	11.4	Viable Option
Ni-Cr Mesh	0.25 mm	0.4	Too Rigid



Mechanical: SMP Characterization



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Epoxy SMP Formulation

0.02 mol (7.28g) EPON 826

0.01 mol (2.3g) Jeffamine D230

100°C for 1.5hr, 130°C for 1hr

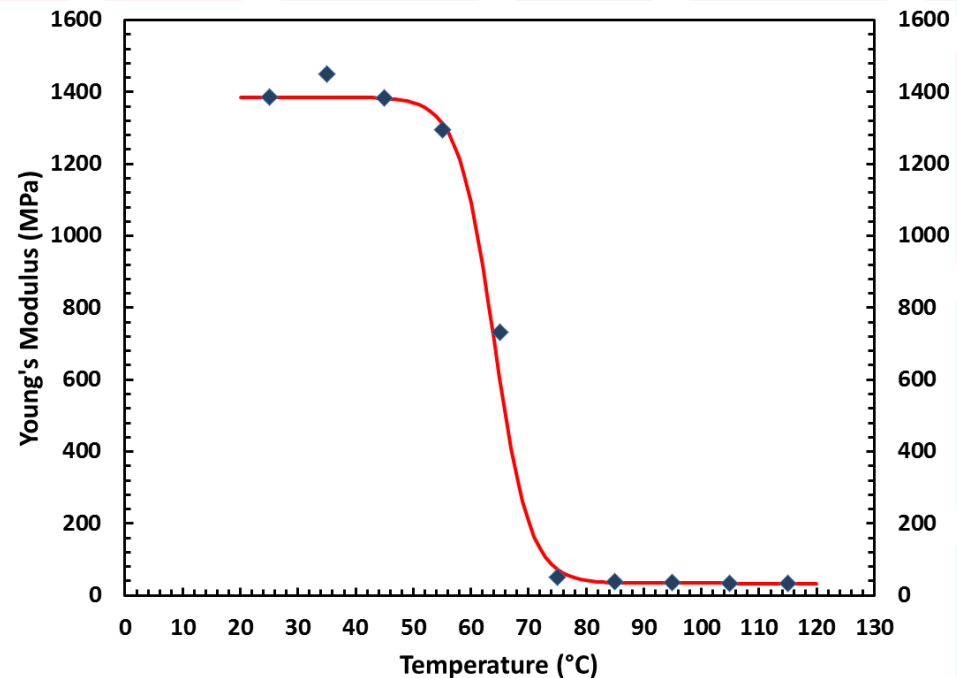


Epoxy SMP Characterization

Experimental Results

T_g	65 °C
E (ambient)	1400 MPa
E (115 °C)	32 MPa

Values consistent over several batches, 0-8 week sample age

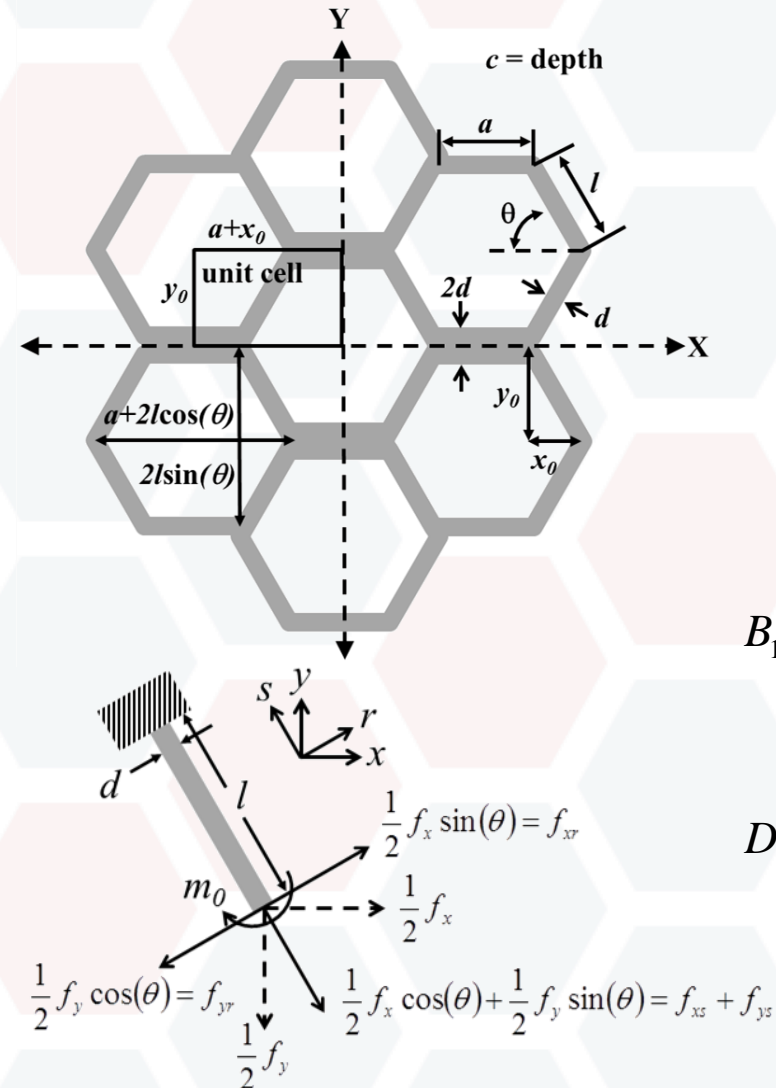




Mechanical: System Mechanics Model

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Filled Honeycomb Mechanics – In-plane Modulus



Literature Models

$$E_{cx} = B_1 E_h + B_2 E_i$$

$$E_{cy} = D_1 E_h + D_2 E_i$$

B_1, D_1 calculated using strain energy and deformation of honeycomb

B_2, D_2 calculated using strain energy from deformation of infill

Deformation of infill and honeycomb matched to give E_{cx} and E_{cy}

$$B_1 = \frac{12I(a + x_0)}{c l y_0^2 \left(y_0 + \frac{12I \cos^2(\theta)}{y_0 A} + \frac{6Ia}{y_0 l A} \right)}$$

$$B_2 = \frac{(a + x_0)K}{2y_0 \beta^2 (1 - \nu_i^2)}$$

$$D_1 = \frac{12I y_0}{c(a + x_0) \left(l x_0^2 + \frac{12I y_0 \sin(\theta)}{A} \right)}$$

$$D_2 = \frac{y_0 K}{2(a + x_0)(1 - \nu_i^2)}$$

$$K = \beta^3 - \gamma \beta^3 + \frac{\gamma^2 \beta^3}{2} \ln \left(1 + \frac{2}{\gamma} \right) + \frac{1}{\beta} + \frac{\gamma}{\beta} + 2\nu_i \beta \quad \beta = \frac{y_0}{x_0} \quad \gamma = \frac{a}{x_0}$$



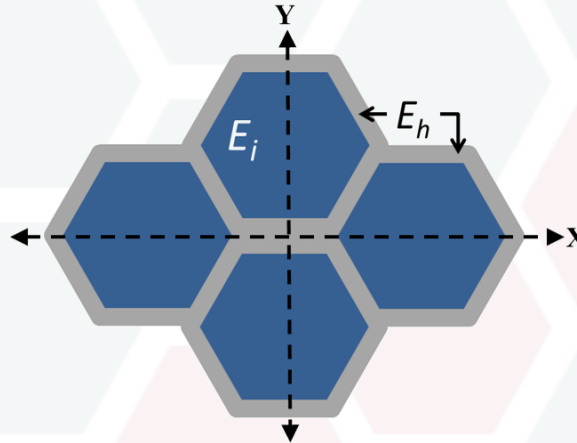
Mechanical: System Mechanics Model



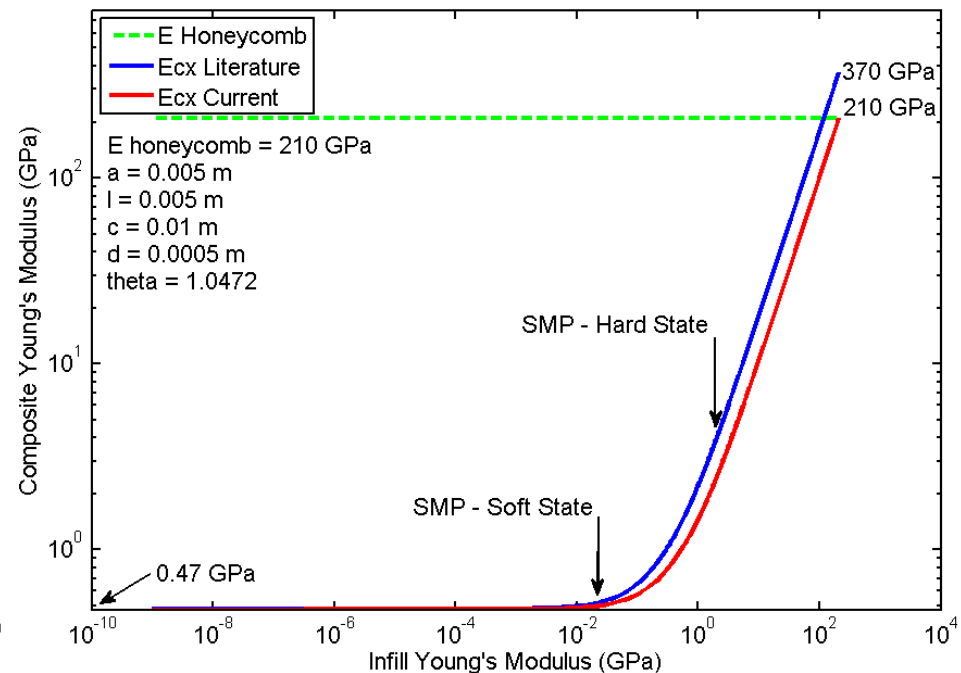
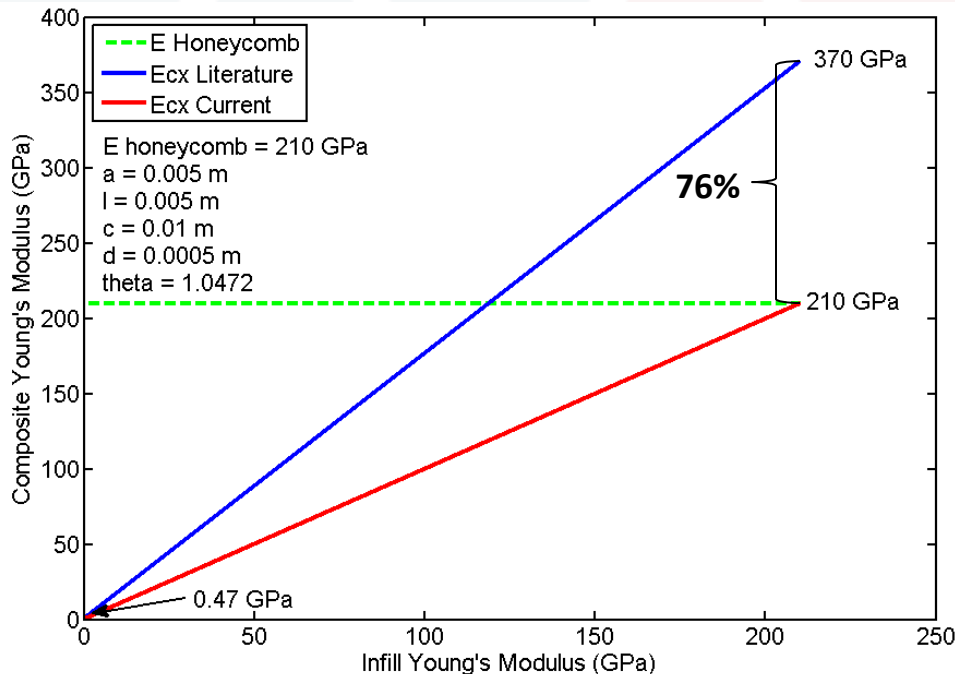
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Current Model

If $E_i = E_h$
Then $E_{cx} = E_{cy} = E_h$



$$E_{cx} = B_1 E_h + (1 - B_1) E_i$$
$$E_{cy} = D_1 E_h + (1 - D_1) E_i$$



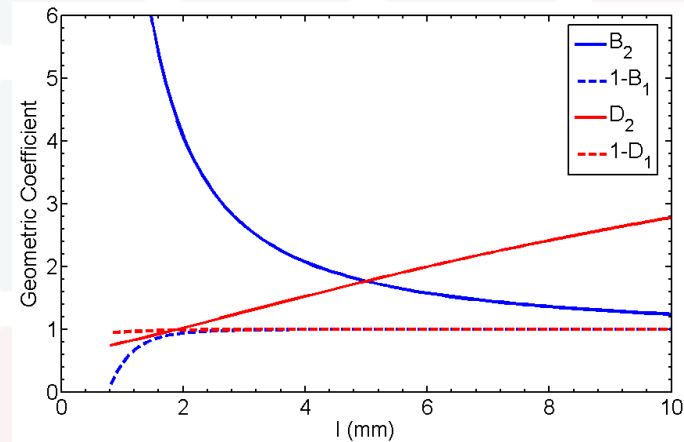
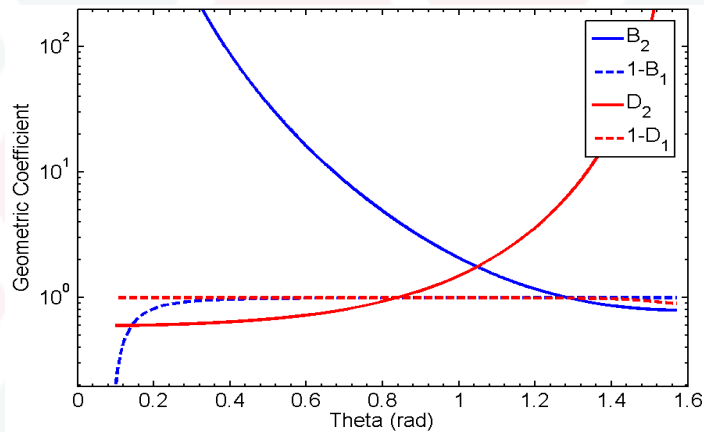
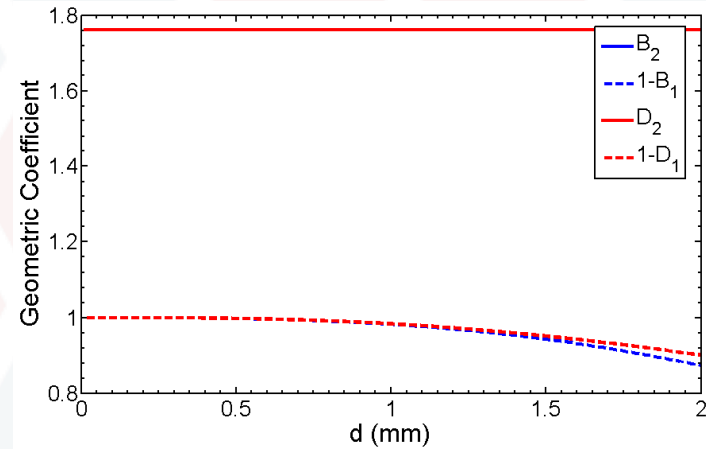
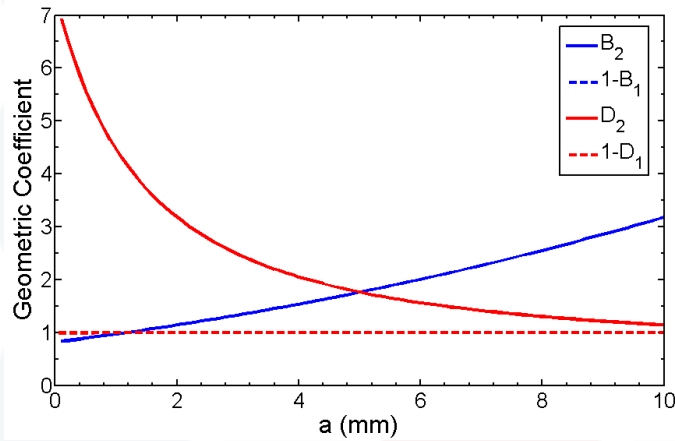


Mechanical: System Mechanics Model



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$$E_{cx} = B_1 E_h + (1 - B_1) E_i \quad E_{cy} = D_1 E_h + (1 - D_1) E_i$$





System Effort: Geometry Optimization



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Geometry/Environment

Plate: 0.508 x 0.381 m

Load: 19 kN/m²

Matlab Optimtool Constraints

$\delta = 2.5$ mm

$55^\circ \leq \theta \leq 75^\circ$

$d \geq 0.2$ mm

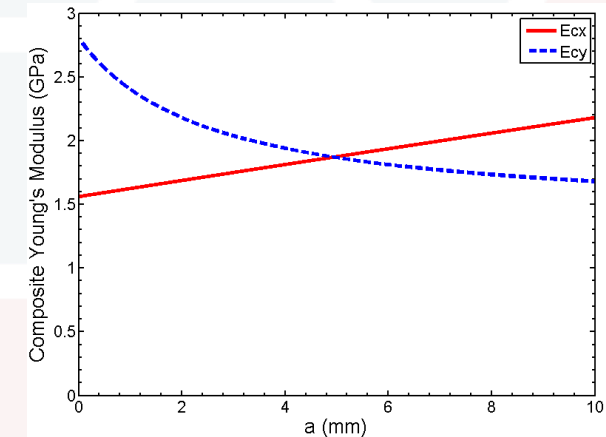
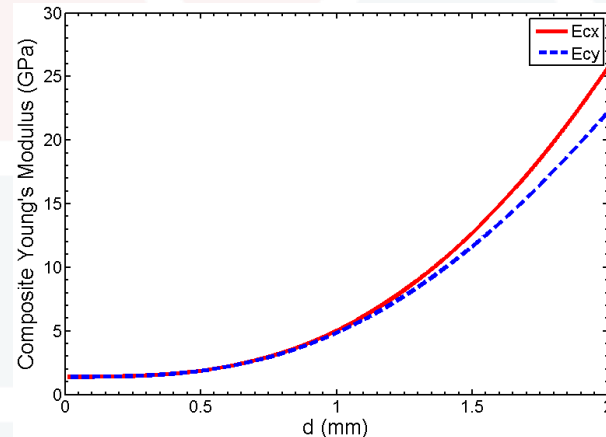
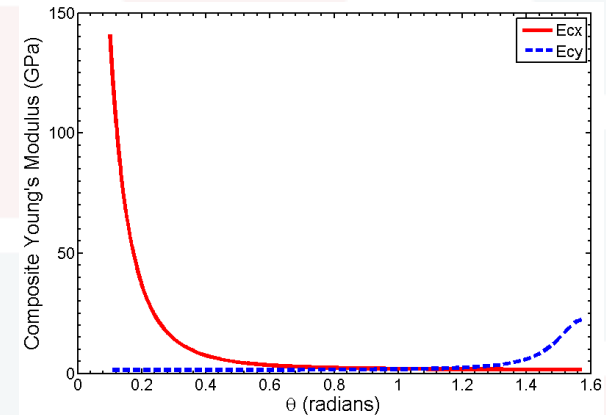
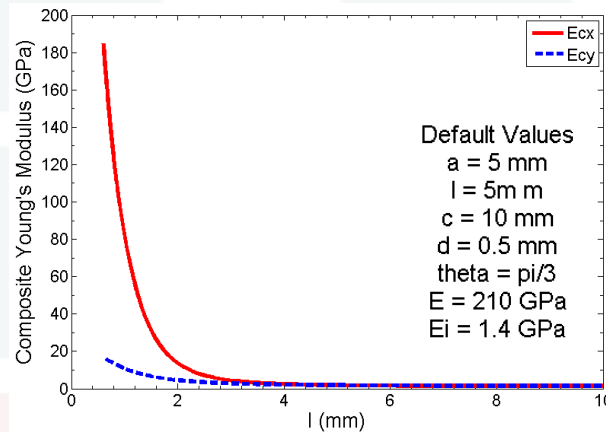
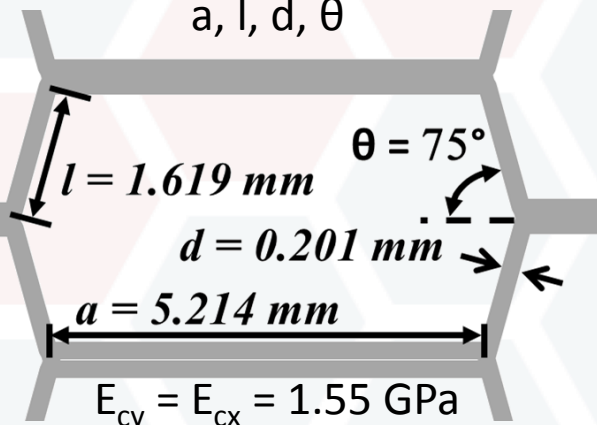
$l, a \leq 100$ mm

Objective Function

$$\text{Min}(E_{cx} + E_{cy})$$

Design variables

a, l, d, θ



Influence of Design Variables



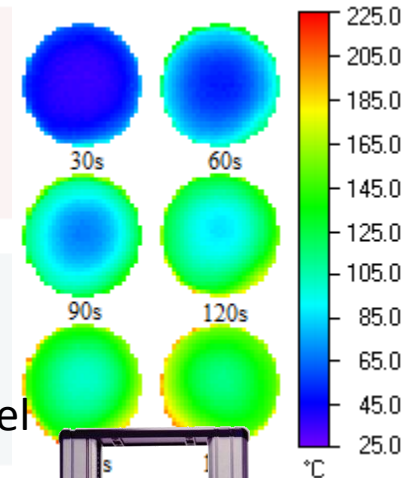
Future Work



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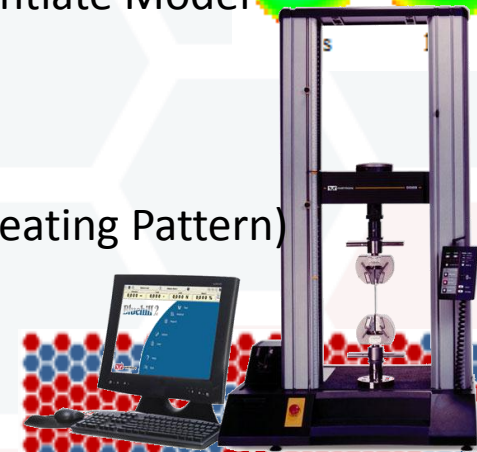
Thermal

Aligned Nickel Particle Electrical Resistance
Thermal Imaging (Speed and Uniformity of Heat)



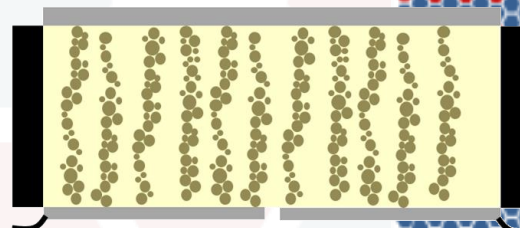
Mechanical

Static Testing of Various Geometries of Honeycomb to Substantiate Model
Static Testing of Filled Honeycombs
Add Shear Modulus and Poisson's Ratio to Geometry Model
Continue Refinement of Optimization Model
FEA Analysis of Filled Honeycomb (Single Cell and Sheet w/ Heating Pattern)



System

Optimization of Multiple Reconfigurable Shapes
Fabrication of Entire System (Flexible Electrodes, Wiring, etc.)
Scaled Pressure Test of Optimized System





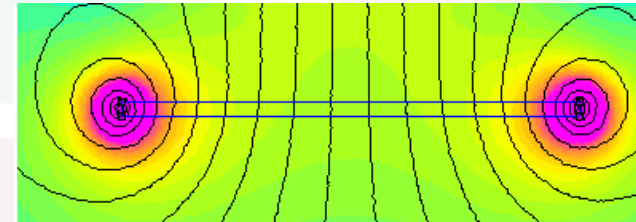
Summary



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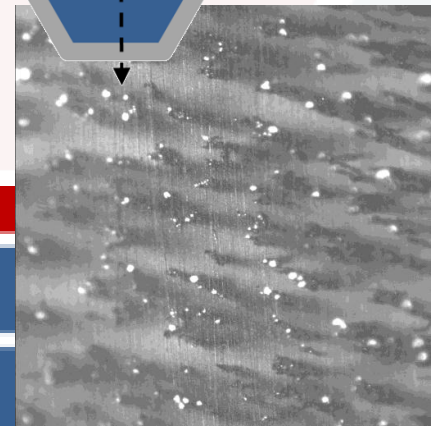
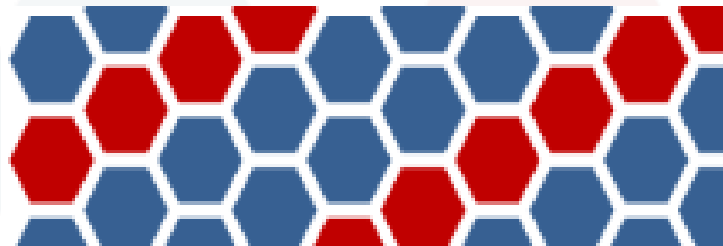
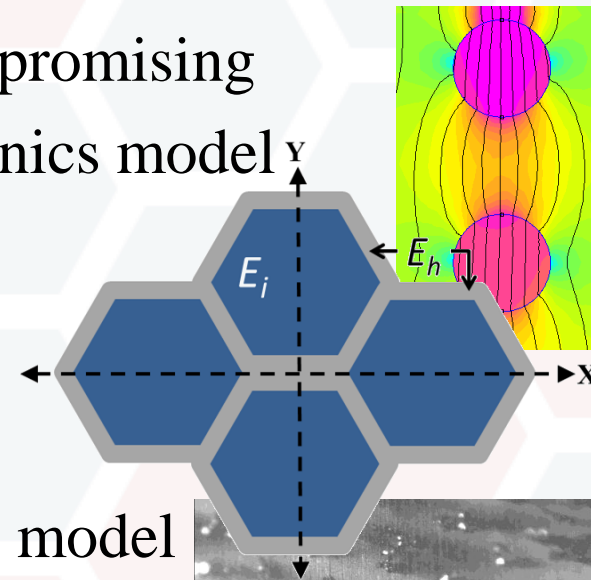
Major Milestones

- Characterization of custom SMP
- Thermal model suggests densely packed small wire-like heaters
- Magnetically aligned particle chain heaters promising
- Promising, more accurate composite mechanics model
- Optimization underway of unit cell



Major Challenges

- System integration/wiring/manufacturing
- Composite testing substantiating mechanics model
- Optimization of composite/cell heating pattern





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Thank You

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